

# Phase Transfer Catalysis in Polycondensation Processes. IX. Study on Polyetherification of 3,3-bis (chloromethyl) Oxetane and Bisphenol A

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## ABSTRACT

The polycondensation of 3,3-bis (chloromethyl) oxetane (BCMO) with bisphenol A (BPA) under the phase transfer conditions is investigated. Second order, central, composite, rotatable experimental design is used in order to carry out this work and to mark limits of the experimental field for better yields and stable mesophase on a large domain.

## Key Words

polyetherification, phase transfer catalysis, liquid-crystals, experimental design, bisphenol A, 3,3-bis (chloromethyl) oxetane

## INTRODUCTION

Phase transfer catalysis (PTC) has been widely used in synthesis of various polymers [1-5]. Good results were obtained in preparation of polymers with ordered structure which might display liquid - crystalline (LC) properties [1,3,4].

In a previous paper [3], we have reported the possibility of obtaining polyethers from 3,3-bis

(chloromethyl) oxetane (BCMO) and bisphenol A (BPA) under phase transfer conditions and we found that these polymers have anisotropic properties in the molten state.

Here results are presented concerning the influence of various parameters, both on reaction conditions and on the most important LC

## EXPERIMENTAL

### Materials

BCMO was prepared according to the method presented in [2]. Commercial bisphenol A (CAROM S.A.) was twice recrystallised from benzene. The PT catalyst (triethyl benzyl ammonium chloride - TEBAC) was prepared in the laboratory from triethylamine and benzylchloride and purified by usual methods. Nitrobenzene (Merck) was used as purchased.

The polyethers were synthesised as in [3]. Transition temperatures (structural ( $T_s$ ) and isotropisation ( $T_i$ ) temperatures) were measured on a VEB analytic optical polarised microscope equipped with a hot stage.

### Experimental Design

To carry out the work, the second order, central, composite, rotatable experimental design was used [7].

The advantages of this method are:

- the number of experiments is reduced, a fact which results in the reduction of the amount of material, energy and time spent;
- the regression equation obtained by data processing is defined on the whole experimental field;
- the complexity of calculation of regression coefficients is reduced due to the orthogonality of many independent variables vectors.

Actual independent variables were

transformed according to the following formula:

$$x_i = (x_i - x_{ic})/\Delta x_i \quad (1)$$

where  $x_i$  = encoded variable, dimensionless

$x_i$  = actual variable

$x_{ic}$  = central value for "i" variable

$\Delta x_i$  = factorial interval for "i" variable.

Variable transformation is given in Table 1, and experimental conditions are listed in Table 2.

### Data Processing

The experimental results were processed by using a multiple regression method in order to obtain response surfaces in the form:

$$Y = a_0 + \sum a_i x_i + \sum a_{ij} x_i x_j \quad (i \leq j) \quad (2)$$

where  $a_i$  and  $a_{ij}$  are the regression coefficients for the property Y.

To perform the calculus standard subroutines which compute regression coefficients from equation (2), together with the statistics necessary to test their significance and the regression significance were used.

The obtained response surfaces were studied to give the influence of reaction parameters (reaction temperature, concentration of TEBAC, concentration of NaOH and reaction time) on the polyetherification of BCMO with BPA.

## RESULTS AND DISCUSSION

To understand the influence of the studied

Table 1. Transformation of variables.

Coded values	-2	-1	0	1	2
Real values					
Polymerisation time ( $X_1$ )[h]	3	5	7	9	11
Reaction temperature ( $X_2$ )[°C]	60	68	76	84	92
Concentration of NaOH ( $X_3$ ) [equivalent/L]	4	8	12	16	20
PT catalyst ( $X_4$ ) [mmol]	0.8	1.6	2.4	3.2	4.0

Table 2. Experimental design and experimental results.

No.	X <sub>1</sub>	X <sub>2</sub>	X <sub>3</sub>	X <sub>4</sub>	Conv. (%)	T <sub>1</sub> (°C)	T <sub>2</sub> (°C)
1	-1	-1	-1	-1	5.0	223	228
2	+1	-1	-1	-1	8.9	222	229
3	-1	+1	-1	-1	34.4	218	223
4	+1	+1	-1	-1	77.6	237	247
5	-1	-1	+1	-1	3.7	224	226
6	+1	-1	+1	-1	7.7	220	227
7	-1	+1	+1	-1	37.8	210	219
8	+1	+1	+1	-1	72.3	240	245
9	-1	-1	-1	+1	6.3	224	230
10	+1	-1	-1	+1	31.8	205	212
11	-1	+1	-1	+1	40.1	215	225
12	+1	+1	-1	+1	86.7	243	251
13	-1	-1	+1	+1	8.7	226	230
14	+1	-1	+1	+1	9.1	220	226
15	-1	+1	+1	+1	84.8	243	259
16	+1	+1	+1	+1	85.3	236	250
17	-2	0	0	0	18.4	212	217
18	+2	0	0	0	36.8	208	215
19	0	-2	0	0	0.8	197	200
20	0	+2	0	0	96.0	248	255
21	0	0	-2	0	8.1	220	223
22	0	0	+2	0	24.7	210	217
23	0	0	0	-2	17.6	210	217
24	0	0	0	+2	81.8	237	250
25	0	0	0	0	26.5	210	217
26	0	0	0	0	28.9	210	218
27	0	0	0	0	29.2	209	215
28	0	0	0	0	29.4	209	217
29	0	0	0	0	28.9	210	217
30	0	0	0	0	27.8	210	218
31	0	0	0	0	32.5	211	217

parameters on the progress of the polyetherification process, Figure 1 represents the variation of the polymer yield versus a parameter, all the others being taken at values corresponding to the center of the experimental field.

The shape of these curves assert a significant influence of reaction temperature (X<sub>2</sub>) and concentration of the PT catalyst (X<sub>4</sub>) for values which exceed 0.15 mmol/L. The improvement of the polymer yield at high concentrations of the catalyst is presumed to result from the increase of

BPA transferred in the organic phase. One should note also that for the selected experimental domain, the conversion curve retains a maximum, which corresponds to a concentration of NaOH of 13.5 N (X<sub>3</sub> = 0.378378). For higher concentrations, a slight decrease in the yield is observed and is justified by the transfer of HO<sup>-</sup> ions in the organic phase. Here they compete with bisphenolate ions in modifying part of -CH<sub>2</sub>Cl groups into -CH<sub>2</sub>OH ones which are less active polyetherification:

Such a phenomenon was notified also for

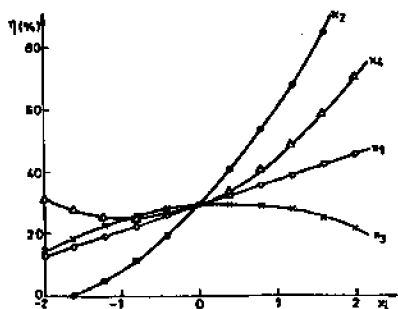
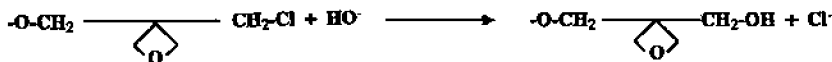


Fig.1. Influence of independent variables upon conversion.

other PT assisted polyetherification reaction [8,9].

The shape of the curves representing the variation of conversion in the experimental field of  $X_1$  and  $X_4$ , shows that at low temperatures, evolution of the polymer yield depends dominantly upon reaction time. This subordination modifies when  $X_1$  and  $X_4$  overtake the middle of the experimental domain.

The examination of concomitant influence of these variables upon conversion is not significant (Figures 2,3 and 4). Moreover, drawings in the plane of two parameters assert that the yield evolution is mainly dependent on the reaction

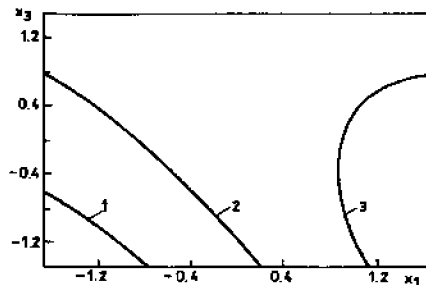


Fig.3. Conversion curves in the plane of variables  $X_1X_3$  for:  $\eta = 6.5\%$  (curve 1);  $\eta = 21.2\%$  (curve 2);  $\eta = 35.9\%$  (curve 3).

temperature (Figures 2,5 and 6).

Figures 7 illustrates the influence of the four independent variables upon  $T_p$ . All the curves pass through a minimum which is placed somewhere on the left side of the experimental domain.

Taking into account the individual influences of the selected parameters upon  $T_i$  (a significant characteristic for LC structures), one obtains the representation in Figure 8. All drawings reveal a minimum located before the center of the experimental field. In this zone the polymer yield

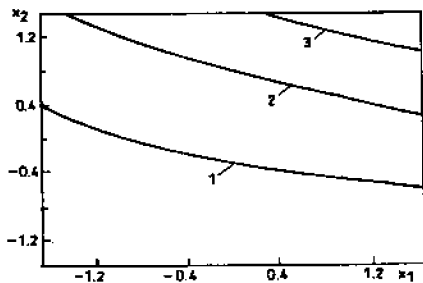


Fig.2. Conversion curves in the plane of variables  $X_1X_2$  for:  $\eta = 20.8\%$  (curve 1);  $\eta = 50.9\%$  (curve 2);  $\eta = 80.0\%$  (curve 3).

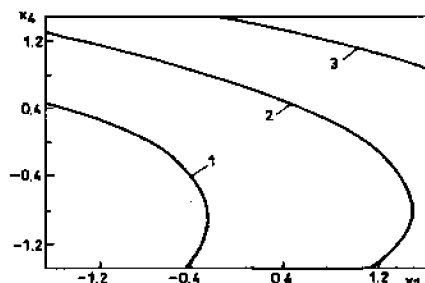


Fig.4. Conversion curves in the plane of variables  $X_1X_4$  for:  $\eta = 22.2\%$  (curve 1);  $\eta = 37.5\%$  (curve 2);  $\eta = 52.9\%$  (curve 3).

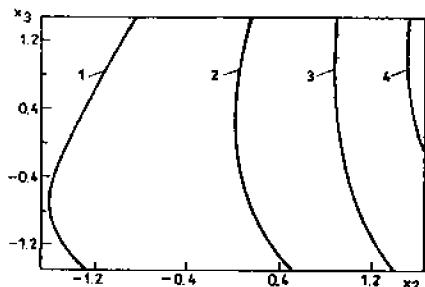


Fig.5. Conversion curves in the plane of variables  $X_2X_3$  for:  $\eta = 1.7\%$  (curve 1);  $\eta = 29.1\%$  (curve 2);  $\eta = 56.4\%$  (curve 3);  $\eta = 83.7\%$  (curve 4).

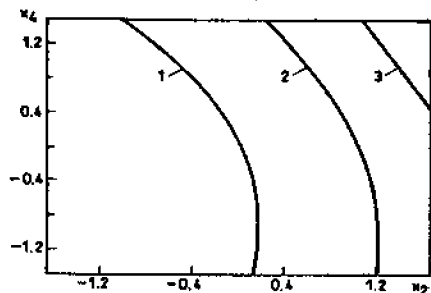


Fig.6. Conversion curves in the plane of variables  $X_2X_4$  for:  $\eta = 28.1\%$  (curve 1);  $\eta = 59.7\%$  (curve 2);  $\eta = 91.3\%$  (curve 3).

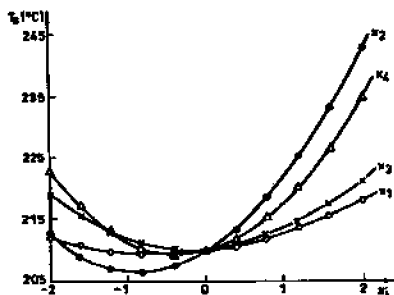


Fig.7. The influence of independent variables upon  $T_1$ .

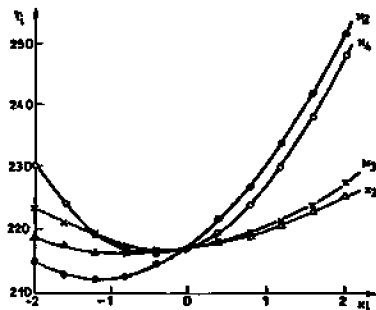


Fig.8. The influence of independent variables upon  $T_1$ .

does not exceed 30%.

It is worth mentioning that the most important evolution of the conversion occurs in the second part of the experimental domain, and that, among the four parameters,  $X_2$  and  $X_4$  have an ascendancy over the  $X_1$  and  $X_3$ .

The isotropisation temperature depends more on  $X_2$  than on  $X_1$ , especially when real values of  $X_2$  are higher than 80 °C (Figure 9).

No major influence is seen from reaction time ( $X_1$ ) and concentration of NaOH ( $X_3$ ) upon isotropisation temperature. It rises only by 16 °C for the entire domain of  $X_1$  and  $X_3$ .

By comparing representations in Figures 7 and 8, the following order of the independent

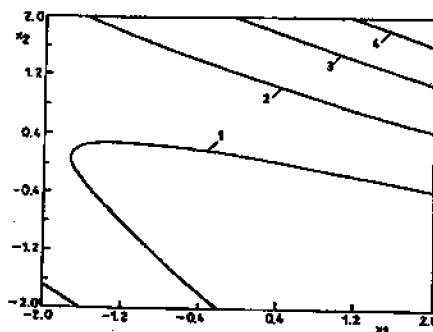


Fig.9. Variation of  $T_1$  as function of variables  $X_1X_2$  for:  $T_1 = 217.6$  °C (curve 1);  $T_1 = 233.6$  °C (curve 2);  $T_1 = 249.7$  °C (curve 3);  $T_1 = 265.8$  °C (curve 4).

variables can be established as they influence the polyetherification process:  $X_2 > X_4 > X_3 > X_1$ .

## CONCLUSIONS

A second order, central, composite, rotatable experimental design was used to study the influence of polyetherification period, temperature, PT catalyst and NaOH concentrations on the polycondensation of BCMO with BPA.

From the obtained data, it results that the most important factors are reaction temperature and concentration of the PT catalyst.

These investigations allowed us to mark better limits of the experimental field in order to obtain good yields and stable mesophases on a large domain.

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